

We know from before that

$$e^{j\theta} = \frac{A+D}{2} + j \left[1 - \left(\frac{A+D}{2} \right)^2 \right]^{1/2} = \cos\theta + j\sin\theta.$$

$$\Rightarrow \theta = \cos^{-1} \left(\frac{A+D}{2} \right) = \cos^{-1} \left(1 - \frac{d}{f_2} \right)$$

$$f_2 = \frac{2}{3}d \Rightarrow \theta = \cos^{-1} \left(1 - \frac{3}{2} \right) = \cos^{-1} \left(-\frac{1}{2} \right) = \frac{2\pi}{3} (120^\circ).$$

\therefore our solution for the position r is given by

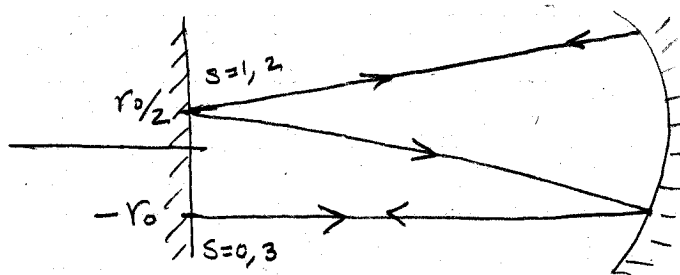
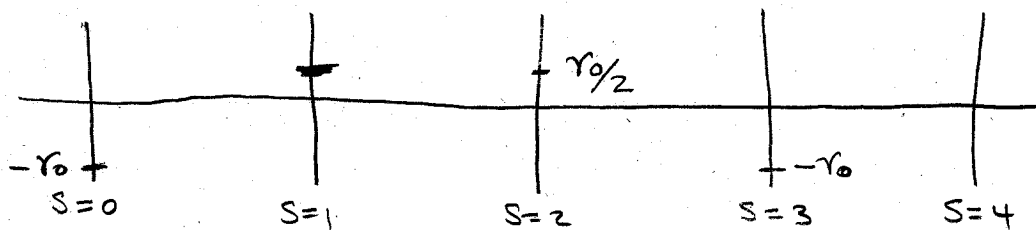
$$r = r_{\max} \sin \left(s \frac{2\pi}{3} + \alpha \right)$$

$$\text{at } s=0 \quad r_{\max} \sin \alpha = -r_0 =$$

$$\sin \alpha = -1. \quad r_{\max} = r_0,$$

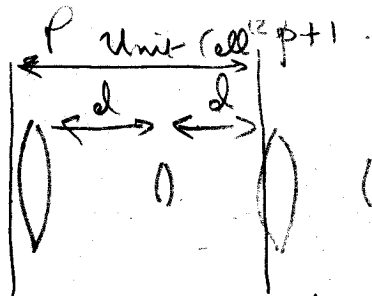
$$\alpha = -\frac{\pi}{2}$$

$$r = r_0 \sin \left(s \frac{2\pi}{3} - \frac{\pi}{2} \right). \quad (\text{location on } M_1)$$



If we want to know locate at other minor M_2

we can use a different unit cell.



Solution $r = 2r_0 \sin \left(p \frac{2\pi}{3} - \frac{\pi}{6} \right)$

Different choices of unit cell \Rightarrow different solutions and information only about the position at the edge of that unit cell.

Repetitive Ray Paths.

- How many round trips before the ray returns to its original position?

$$r_s = r_{max} (\sin \theta + \alpha)$$

$$\theta = \cos^{-1} \left(\frac{A+D}{2} \right)$$

For repetitive m round trips is required where $m\theta = 2n\pi$ - some multiple of 2π .

$$n < \frac{m}{2}$$

$$m = \frac{2\pi n}{\theta} \quad \text{for } \theta = \frac{2\pi}{3} \quad m = 3n$$

$$n < \frac{m}{2}$$

$n=1, m=3$ is a solution.

Initial Conditions - Stable cavity.

If cavity is stable $\theta = \cos^{-1}\left(\frac{A+D}{2}\right)$. $\cos\theta = \left(\frac{A+D}{2}\right)$

Suppose initial conditions are r_0 and r_0'

$$r = |r_{\max}| \sin(s\theta + \alpha)$$

$$s=0$$

$$r = |r_{\max}| \sin(\alpha) = r_0$$

After 1 round trip:

$$r_1 = A r_0 + B r_0' = |r_{\max}| \sin(\theta + \alpha)$$

$$A r_0 + B r_0' = |r_{\max}| \sin(\theta + \alpha)$$

$$= |r_{\max}| (\sin\theta \cos\alpha + \cos\theta \sin\alpha)$$

$$= |r_{\max}| \sin\theta \cos\alpha + |r_{\max}| \frac{A+D}{2} \sin\alpha$$

$$= |r_{\max}| \sin\theta \cos\alpha + r_0 \frac{(A+D)^2}{2}$$

$$|r_{\max}| \cos\alpha = \frac{1}{\sin\theta} \left[r_0 \left(\frac{A-D}{2} \right) + B r_0' \right]$$

$$\text{We have } |r_{\max}| \sin\alpha = r_0$$

$$\tan\alpha = \frac{r_0 \sin\theta \left[r_0 \left(\frac{A-D}{2} \right) + B r_0' \right]^{-1}}{r_0}$$

$$\text{but } \sin\theta = \left(1 - \left(\frac{A+D}{2} \right)^2 \right)^{1/2}$$

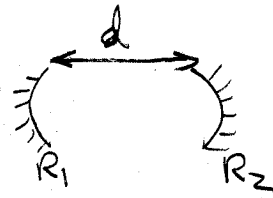
$$\tan\alpha = \left[\frac{r_0 \left(1 - \left(\frac{A+D}{2} \right)^2 \right)^{1/2}}{r_0 \left(\frac{A-D}{2} \right) + B r_0'} \right]$$

Once α is determined

$$|r_{\max}| = \frac{r_0}{\sin\alpha}$$

$$\textcircled{1} \tan \alpha = \left[\frac{r_0 \left(1 - \left(\frac{A+D}{2} \right)^2 \right)^{1/2}}{r_0 \frac{(A-D)}{2} + B r_0'} \right]$$

Review Stability Criteria



$$0 \leq g_1, g_2 \leq 1$$

$$g_{1,2} = 1 - \frac{d}{R_{1,2}}$$

Solution for stable system $r = r_{\max} \sin(s\theta + \alpha)$
 where s is the number of round trips.

Unstable Cavities

Recall difference equation is of form

$$r_{s+2} - 2 \left(\frac{A+D}{2} \right) r_{s+1} + r_s = 0.$$

For unstable cavities, solution is of the form

$$r_s = r_0 (F)^s$$

both solutions are real.

$$F_{1,2} = \frac{A+D}{2} \pm \left[\left(\frac{A+D}{2} \right)^2 - 1 \right]^{1/2}$$

General solution $r_s = r_a (F_1)^s + r_b (F_2)^s$

Unstable cavities $\frac{A+D}{2} \geq 1$ or $-1 \geq \frac{A+D}{2}$

remember $\cos \theta$ for stable cavities.

$\Rightarrow F_1$ or F_2 has a magnitude > 1 and thus after a few round trips the solution is approximately

$$r_s \sim r_0 (F_2)^s$$

\approx largest solution.

Evaluation of r_a & r_b .

$S=0 \quad r_s = r_a + r_b = r_0$

$S=1 \quad r_i = r_a F_1 + r_b F_2 = A r_0 + B r_0'$

Solving for r_a and r_b yields:

$$r_b = \frac{1}{F_1 - F_2} (r_0 (F_1 - A) - B r_0')$$

$$r_a = \frac{1}{F_2 - F_1} (r_0 (F_2 - A) - B r_0')$$

So far we have discussed ray tracing in homogeneous material systems. What happens in inhomogeneous, or lenslike media.

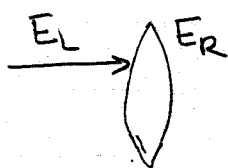


plano-convex

thickness causes changes to our simple rounded picture.

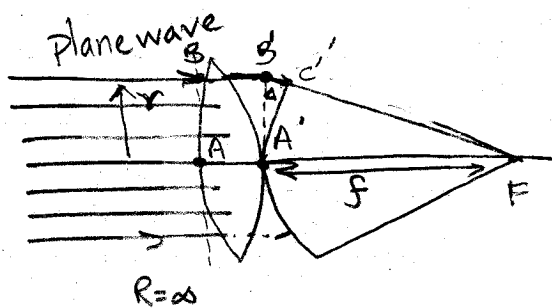
For example.

lens - constant index - quadratic physical path.



$$E_R(x,y) = E_L(x,y) e^{\frac{ik(x^2+y^2)}{2f}}$$

How do we get this?



If the lens is not there B' & A' would be in phase, however A' and C' are in phase.

recall $v = \frac{c}{n}$.

$E \propto e^{-jkz}$ for right going wave

$k = \frac{2\pi}{\lambda} = \frac{2\pi n}{\lambda_0}$ ← index causes phase difference

$\Delta = \overline{FB'} - \overline{FC'}$

$\overline{FB'} = \sqrt{r^2 + f^2} \quad \overline{FC'} = f$

$$\Delta = \overline{FB'} - \overline{FC'} = \sqrt{r^2 + f^2} - f = f \sqrt{1 + \frac{r^2}{f^2}} - f.$$

$$\sqrt{1 + \frac{r^2}{f^2}} \approx 1 + \frac{r^2}{2f^2} \quad 49$$

if $f \gg r$ (paraxial approximation).

$$\Delta \approx f \left(1 + \frac{r^2}{2f^2}\right) - f = \frac{r^2}{2f} = \frac{x^2 + y^2}{2f}$$

phase difference $\equiv \# \lambda \times 2\pi = \frac{\text{path difference}}{\lambda} \times 2\pi = \Delta \times \frac{2\pi}{\lambda}$

$$\Rightarrow E_R(x, y) = E_L(x, y) e^{ik\Delta} = E_L(x, y) e^{ik \left(\frac{x^2 + y^2}{2f}\right)}$$

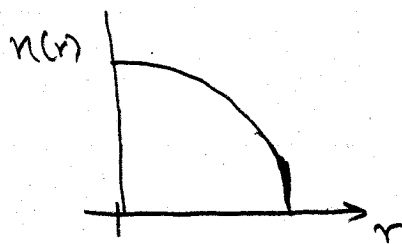
$v = \frac{c}{n}$ - wave inside glass is moving slower.

Another example.

$$n(r) \sim r^2 \quad (\text{distance from center}).$$

eg. $n(x, y) = n_0 \left[1 - \frac{k_2}{2k} (x^2 + y^2) \right]$ $k_2 = \text{constant of material}$

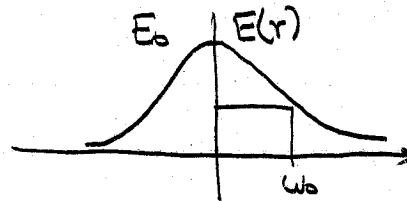
1. graded index fiber.



2. propagation of intense laser beam through a medium with $n = n(I)$.

$$n = n_0 + n_2 I$$

Gaussian spatial profile



$$I(r) = I_0 e^{-2 \left(\frac{r}{w_0}\right)^2}$$

$w_0 = \text{half width at } \frac{E_0}{e}$.

paraxial approx:

$$I(r) = I_0 \left[1 - 2 \left(\frac{r^2}{w_0^2} \right) \right]$$

$$r \ll w_0$$

50/

$$\Rightarrow n = \underbrace{n_0 + n_2 I_0}_{n'_0} - \frac{2n_2 r^2}{w_0^2}$$

where n_2 is a constant of the material.

$$= n'_0 - 2n_2 \left(\frac{x^2 + y^2}{w_0^2} \right) = n'_0 \left[1 - \frac{2n_2}{n'_0 w_0^2} (x^2 + y^2) \right]$$

→ Gaussian beam propagating in weakly absorbing medium (change index due to heating).

$$\frac{dn}{dT} \neq 0$$

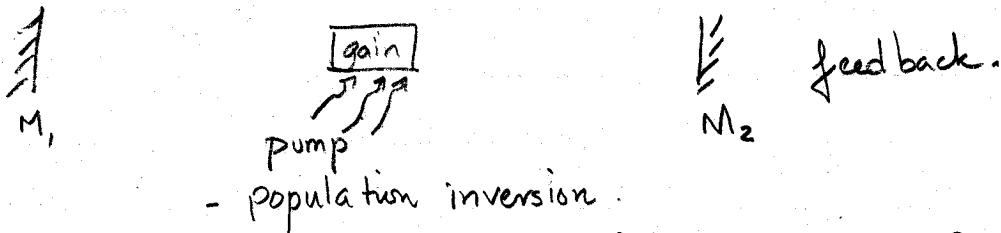
$\frac{dn}{dT} > 0$. (n increases in center of beam relative to wings \Rightarrow converging lens "self focusing".)

$\frac{dn}{dT} < 0 \Rightarrow$ diverging lens "self-defocusing".

(3) Optical pumping of solid state lasers:

3 elements to laser

- ① gain medium
- ② pumping mechanism.
- ③ cavity (resonator).



gain medium : gas, organic dyes, some solid state material
pumping : electrical discharge, chemical reaction, another laser, flash lamps.
Nd:YAG \leftarrow flash lamps
Ti:Sapphire \leftarrow laser.

Energy in gain medium not converted to laser \Rightarrow heat

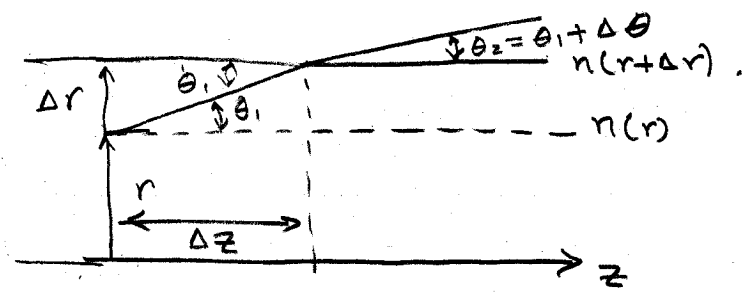
\Rightarrow Temperature gradient

$T(0) > T(r_0)$ temp at center greater than at outside.

$\frac{dn}{dT} \neq 0 \Rightarrow$ lens effect..

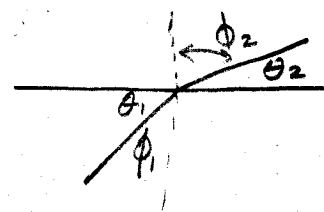
General Differential equation describes propagation through inhomogeneous medium.

Paraxial approximation:



take $\Delta r \rightarrow 0$.

Snell's law of refraction:



$n_1 \sin \phi_1 = n_2 \sin \phi_2$

$n_1 \sin (\frac{\pi}{2} - \theta_1) = n_2 \sin (\frac{\pi}{2} - \theta_2)$

$n_1 \cos (\theta_1) = n_2 \cos (\theta_2)$

so $n(r) \cos (\theta_1) = n(r+\Delta r) \cos (\theta_1 + \Delta \theta)$

expand $n(r)$ in Taylor series.

$n(r+\Delta r) \approx n(r) + \frac{dn}{dr} \Delta r + \dots$

$\cos (\theta_1 + \Delta \theta) = \cos \theta_1 \cos \Delta \theta - \sin \theta_1 \sin \Delta \theta$

$n(r) \cos \theta_1 = [n(r) + \frac{dn}{dr} \Delta r] [\cos \theta_1 \cos \Delta \theta - \sin \theta_1 \sin \Delta \theta]$

for small $\Delta \theta$, $\cos \Delta \theta \approx 1$, $\sin \Delta \theta \approx \Delta \theta$.

$$n(r) \cos \theta_1 = n(r) \cos \theta_1 - n(r) \sin(\theta) (\Delta \theta) + \frac{\partial n}{\partial r} \Delta r (\cos \theta_1 - \Delta \theta \sin \theta_1)$$

$\Delta \theta \rightarrow 0$

$$\Rightarrow n(r) \sin \theta_1 \Delta \theta = \frac{\partial n}{\partial r} \Delta r \cos \theta_1$$

$$\text{or } \frac{\partial n}{\partial r} = n(r) \tan \theta_1 \left(\frac{\Delta \theta}{\Delta r} \right)$$

but paraxial approx: $\tan \theta_1 \approx \frac{\Delta r}{\Delta z}$

$$\frac{\partial n}{\partial r} = n(r) \frac{\Delta r}{\Delta z} \frac{\Delta \theta}{\Delta r} = n(r) \frac{\Delta \theta}{\Delta z}$$

$$\theta_1 \approx \frac{\Delta r}{\Delta z} \Rightarrow \Delta \theta = \Delta \left(\frac{\Delta r}{\Delta z} \right) \Rightarrow \frac{\Delta \theta}{\Delta z} = \frac{\Delta}{\Delta z} \left(\frac{\Delta r}{\Delta z} \right)$$

$$\text{as } \Delta \rightarrow 0 \Rightarrow \frac{\Delta \theta}{\Delta z} \rightarrow \frac{\partial^2 r}{\partial z^2}$$

$$\therefore \frac{\partial n}{\partial r} = n(r) \frac{\partial^2 r}{\partial z^2}$$

$$\boxed{\frac{\partial^2 r}{\partial z^2} = \frac{1}{n(r)} \frac{\partial n(r)}{\partial r}}$$

- solve this equation to describe ray motion in inhomogeneous medium.